Appendix D. Drilled Shaft Report Example

PLEASE NOTE

A sample foundations report is included here for reference. It is provided as an example of content, format, and organization representative of a typical Foundation Investigation and Recommendation Report for a drilled shaft foundation. As site conditions vary widely, the investigation means and methods, and report content (including recommendations), may differ for other projects. Note that the selection and inclusion of this report as a sample does not imply that it is guaranteed to be free of errors. Please contact the Foundations Unit with any questions when interpreting a geotechnical report issued by this office or if you have any questions with respect to preparing geotechnical reports for MnDOT. The information presented here is intended for use as a resource by geotechnical engineering professionals. MnDOT makes no warranty as to the suitability of engineering reports in the style of this sample report, for other geotechnical needs, purposes, clients, or projects.



Minnesota Department of Transportation

Geotechnie 1400 Gerv	Materials & Road Research cal Engineering Section rais Ave - Mailstop 645 od, MN 55109	Office (651) 366-5598 Fax: (651) 366-5510
Date:	October 02, 2008	
То:	D. Dorgan, State Bridge Engineer Office of Bridges & Structures	
From:	Hossana Teklyes, Grad Engineer-2 Foundations Unit	
Concur:	Gary Person, Foundations Engineer Foundations Unit	
Concur:	Rich Lamb, Foundations Project Engineer Foundations Unit	
Subject:	S.P. 3902-21 Bridge 39008 TH 11 over Rapid River in Clementson	
	Preliminary Foundation Investigation and Recommendations	

Project Summary

This report provides for a <u>preliminary</u> foundation investigation, analysis and recommendations for replacing Bridge 5557 with Bridge 39008. The old three-span arch Bridge built in 1950, will be replaced with a new three-span structure. The new Bridge (39008) will use 63 inch prestressed concrete beams with a cast in place deck 40 feet wide by 247 feet long. The substructures are to be supported on drilled shaft foundations.

This report is preliminary in nature because of the iterative design process involved with drilled shaft foundations. A final report will be provided once the final structural loads (both axial and lateral) are determined. Load and Resistance Factor Design (LRFD) methods will be used for the analysis and design recommendations.

Field Investigation and Foundation Conditions

Four foundation borings were taken by STS, under a consultant contract for Mn/DOT, in June 2008. A copy of these borings is included with this report.

West Abutment & Pier

At the proposed west Abutment & Pier the foundation soils consist of a 10-15 ft. layer of sandy clay loam soil followed by bedrock. The bedrock at this site is a greenstone generally fresh with slight weathering. Unconfined compression tests were performed on selected representative rock core samples in order to determine the unconfined compressive strength and elastic modulus of the rock. The results of these tests are plotted on the individual boring logs and are shown in Table 1.Groundwater was not encountered during drilling.

East Abutment & Pier

At the proposed east Abutment & Pier the foundation soils consist of a 15-20 ft. layer of sandy loam soil followed by bedrock. The bedrock at this site is a greenstone generally fresh with slight weathering. Unconfined compressive tests were performed on selected representative rock core samples in order to determine the unconfined compressive strength and elastic modulus of the rock. The results of these tests

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are plotted on the individual boring logs and are shown in Table 1. Groundwater was not encountered during drilling.

West Abutment Samples

Fig 1: Rock Core from 28.1 ft. to 28.4 ft.





East Abutment Samples Fig 3: Rock core from 18.2 ft. to 18.5 ft.



Fig 4: Rock core from 26 ft. to 26.8 ft.



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Fig 2: Rock Core from 40 ft. to 40.3 ft

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Boring	Elevation	Rock Description	q _u psi	elastic modulus, E psi
B-1	1065	Greenstone, slightly weathered	30,000*	3,064,000
B-2	895.3	Greenstone, slightly weathered to generally fresh	30,000*	2,893,100
B-3	897.7	Greenstone, slightly weathered to generally fresh	9,000**	1,825,400
B-4	899.1	Greenstone, slightly weathered to generally fresh	30,000*	3,438,500

 Table 1: Results of Lab Tests on Rock Core Samples

* The rock core did not reach unconfined compressive strength

** The rock core did reach unconfined compressive strength

Please refer to the attached boring logs for a detailed description of the foundation soils and rock. Rock core is available for inspection in our lab. Please contact our office if you wish to see the core.

Foundation Analysis

Locations and elevations of existing and proposed substructures were determined from a bridge survey and a preliminary bridge plan provided by the Bridge Office. The existing three- span arch bridge was constructed in 1950 and is supported on spread footing foundations on the shallow bedrock.

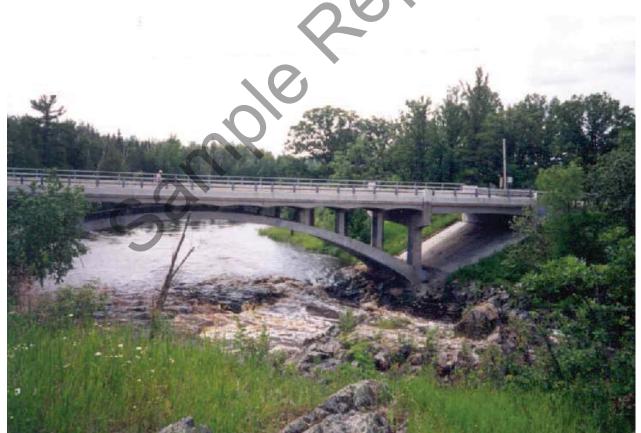


Fig 5.The existing three-span arch Bridge (5557) crossing Rapid River in Clementson

Scour At this site, no scour depth has been predicted by the Hydraulics Section.

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Drilled shaft Settlement

For footings bearing on fair to very good rock, according to the Geomechanics Classification system, as defined in Article 10.4.6.4(AASHTO LRFD Bridge Design Specifications,2008 Interim Revisions), elastic settlements may generally be assumed to be less than 0.5 in.

Lateral loads are not expected to control the drilled shaft design for this project. However, the lateral deflection will be checked once the final structural loads are made available.

The construction method to install the drilled shaft foundations is expected to utilize temporary casing and drilling slurry (water). The casing will first be sealed into competent rock and then the shaft will be drilled out to the design depth. Before placing the rebar cage, the bottom of the shaft will be cleaned out thoroughly.

Abutment & Pier Foundations – Drilled Shaft Axial Capacity

Since bedrock was found at a shallow depth during boring at the abutment and pier locations, drilled shafts foundation were analyzed. Diameters of 36, 42 and 48 in. were assumed for the drilled shaft.

The drilled shaft design follows the guidelines presented in the AASHTO LRFD BRIDGE DESIGN (2008 Interim Revisions). Because of the complexities and unknowns involved with load transfer in stratified rock, a conservative approach was used for design of the axial capacity of the shafts. This design assumes that the axial load will be resisted entirely by side resistance. In actual practice, some of the axial load is transferred to the base of the shaft, however, in lieu of static load testing, it is very difficult to determine how much.

The unit side resistance was first calculated for each material layer using the analysis method of Kulhawy and Phoon (1993).

$$f_{\max i} = 0.65 \alpha = p_a \sqrt{\frac{q_{ui}}{p_a}}$$

where $p_a = atmospheric pressure$ $q_{ui} = unconfined compressive strength of rock$ $\alpha_{E} = reduction factor to account for jointing in rock$

The total side resistance, R_s, was then computed using the following equation:

$$R_s = \phi_s \pi B \sum_{i=1}^n \Delta z_i f_{\max i}$$
 where $\phi_s = 0.55$

Because the final axial and lateral loads are unknown at this time, the factored side resistance is presented as a function of drilled shaft depth and diameter. The Structural Engineer should use this chart to select a preferred shaft diameter and depth and verify that the factored loads, $\eta \Sigma \gamma i Qi$, from the most critical design case (strength or extreme event), meet or exceed the factored resistances for the options shown.

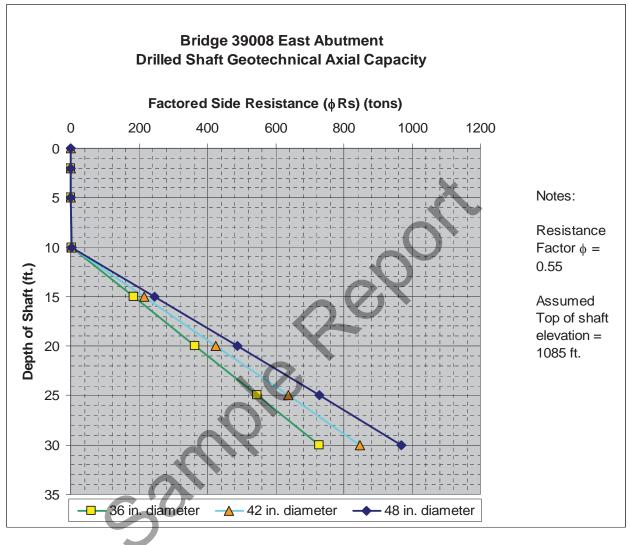


Figure 1: Estimated Factored Geotechnical Side Resistance vs. Depth

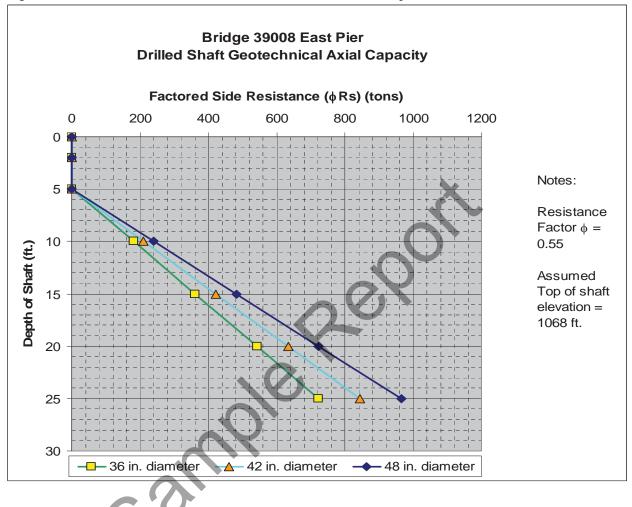


Figure 2: Estimated Factored Geotechnical Side Resistance vs. Depth

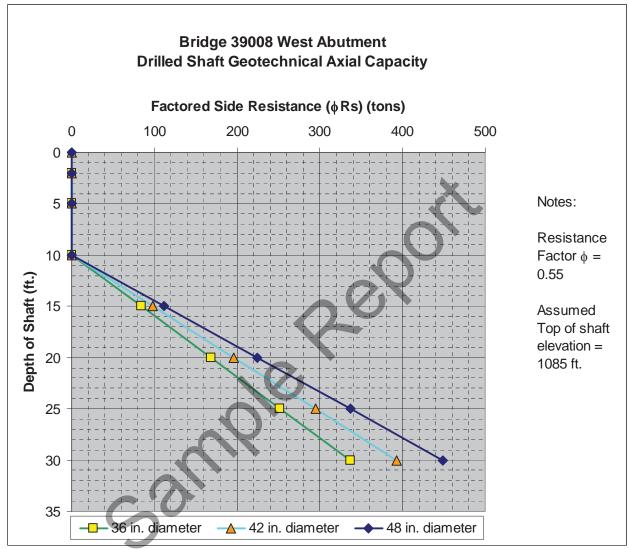


Figure 3: Estimated Factored Geotechnical Side Resistance vs. Depth

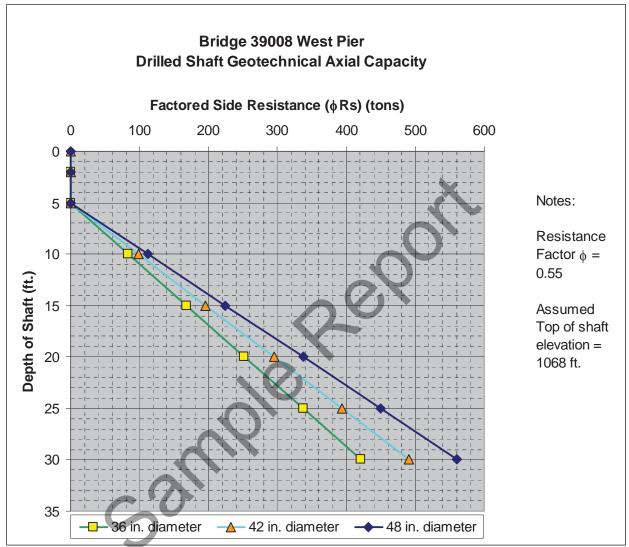


Figure 3: Estimated Factored Geotechnical Side Resistance vs. Depth

Preliminary Foundation Recommendations

Based on the existing conditions along with an analysis of the project soils, we recommend that;

- 1. Topsoil and other organic material should be removed from areas where fill is to be placed.
- 2. The side slopes and end slopes be same as existing or flatter for stability.
- 3. The bridge abutments and piers should be supported with drilled shaft foundations. The drilled shaft diameter and depth will be finalized in the final Foundation Recommendation Report after the final structural loads are made available. Please provide the following loading values to our office when they become available:

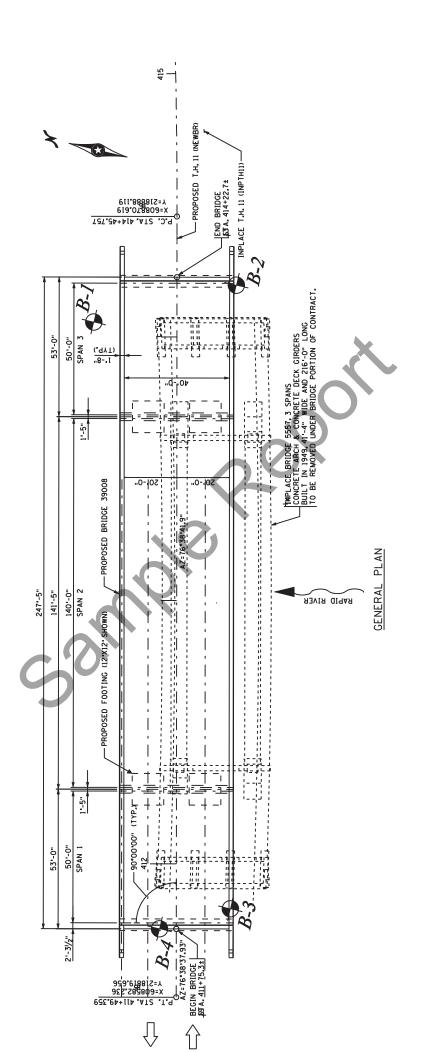
- a. Axial design load per column for most critical design case (strength or extreme event)
- b. Lateral design load per column for most critical design case (strength or extreme event)

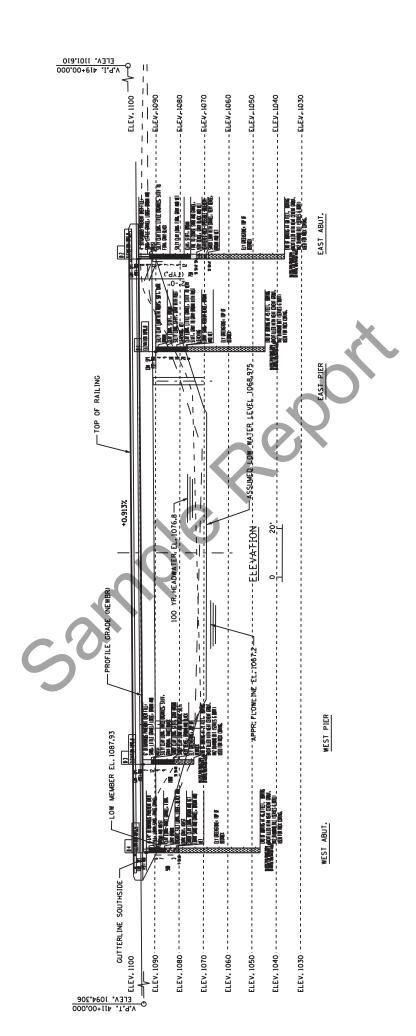
Attachments: Boring Logs B-1 – B-4 (Unique #70658-70661) **Boring Plan Boring Profile**

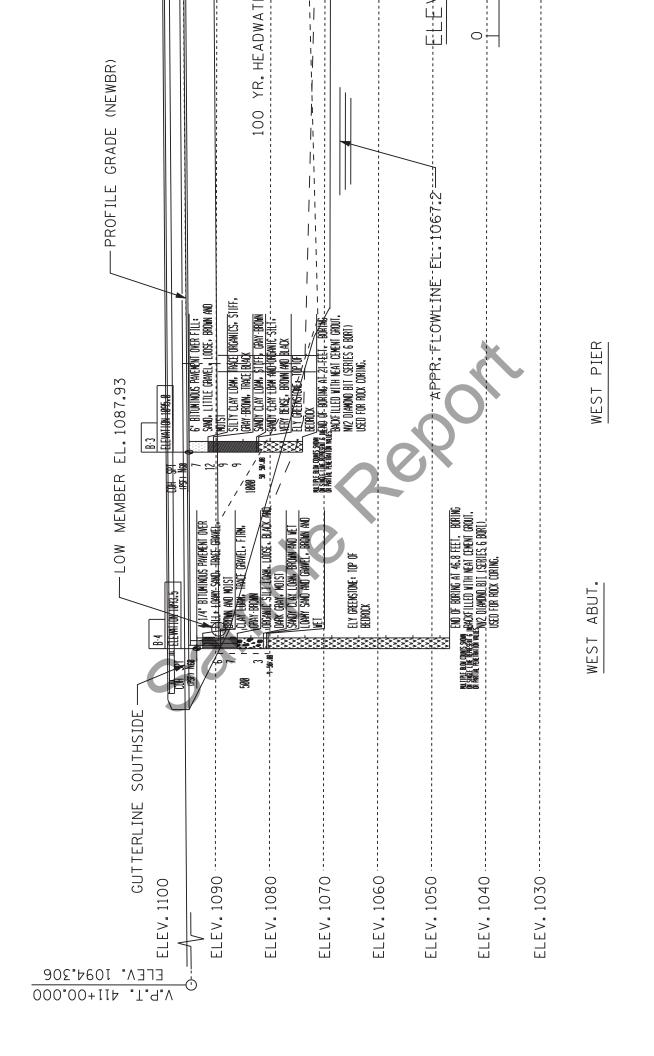
- G. Engstrom cc:
 - D. Dorgan
 - T. Styrbicki
 - A. Staples
- sample D. Robertson
 - J. Bittman

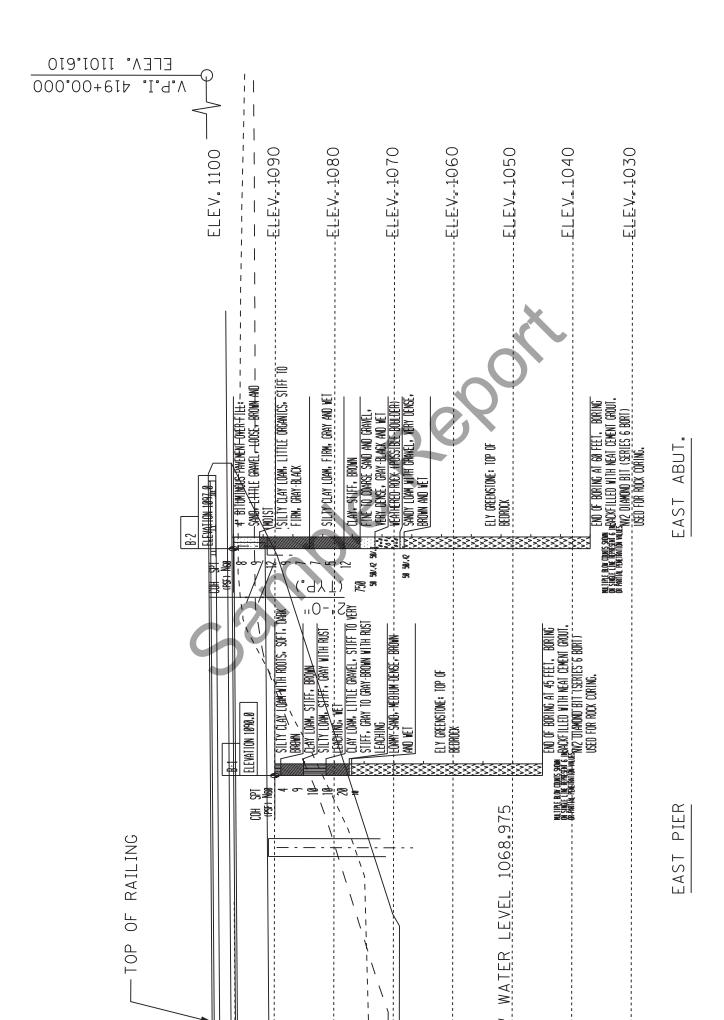
File

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Boring Log Descriptive Terminology (English Units)



USER NOTES, ABBREVIATIONS AND DEFINITIONS - Additional information available in Geotechnical Manual.

This boring was made by ordinary and conventional methods and with care deemed adequate for the Department's design purposes. Since this boring was not taken to gather information relating to the construction of the project, the data noted in the field and recorded may not necessarily be the same as that which a contractor would desire. While the Department believes that the information as to the conditions and materials reported is accurate, it does not warrant that the information is necessarily complete. This information has been edited or abridged and may not reveal all the information which might be useful or of interest to the contractor. Consequently, the Department will make available at its offices, the field logs relating to this boring.

Since subsurface conditions outside each borehole are unknown, and soil, rock and water conditions cannot be relied upon to be consistent or uniform, no warrant is made that conditions adjacent to this boring will necessarily be the same as or similar to those shown on this log. Furthermore, the Department will not be responsible for any interpretations, assumptions, projections or interpolations made by contractors, or other users of this log.

Water levels recorded on this log should be used with discretion since the use of drilling fluids in borings may seriously distort the true field conditions. Also, water levels in cohesive soils often take extended periods of time to reach equilibrium and thus reflect their true field level. Water levels can be expected to vary both seasonally and yearly. The absence of notations on this log regarding water does not necessarily mean that this boring was dry or that the contractor will not encounter subsurface water during the course of construction.

WATER MEASUREMENT

AB	After Bailing	
AC	After Completion	
AF	After Flushing	
w/C	with Casing	
w/M	with Mud	
WSD	While Sampling/D	rilling
w/AUG	with Hollow Stem	Auger

MISCELLANEOUS

NA	Not Applicable
w/	
w/o	. with out
sat	saturated

DRILLING OPERATIONS

DRILLING OF	FERATIONS
AUG	Augered
CD	Core Drilled
DBD	Disturbed by Drilling
DBJ	Disturbed by Jetting
PD	Plug Drilled
ST	Split Tube (SPT test)
TW	Thinwall (Shelby Tube)
WS	Wash Sample
NSR. Index Sheet No.	No Sample Retrieved 3.0 March 2003 G:\geotech\Public\Forms\I

	HUNS - Additional Inic
WH	Weight of Hammer
WR	Weight of Rod
Mud	Drilling Fluids in Sample
CS	Continuous Sample

SOIL/CORE TESTS

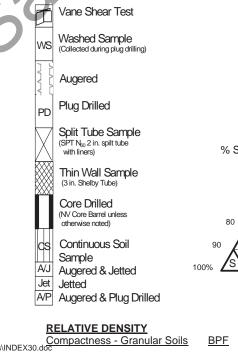
SPT N₆₀ ASTM D1586 Modified Blows per foot with 140 lb. hammer and a standard energy of 210 ft-lbs. This energy represents 60% of the potential energy of the system and is the average energy provided by a Rope & Cathead system. MC..... Moisture Content COH Cohesion y Sample Density LL..... Liquid Limit Pl..... Plasticity Index Φ..... Phi Angle REC..... Percent Core Recovered RQD Rock Quality Description (Percent of total core interval consisting of unbroken pieces 4 inches or longer) ACL Average Core Length (Average length of core that is greater than 4 inches long)

Core Breaks Number of natural core breaks per 2-foot interval.

DISCONTINUITY SPACING

Fractures	Distance	Bedding
Very Close	<2 inches	Very Thin
Close	2-12 inches	Thin
Mod. Close	. 12-36 inches	Medium
Wide	>36 inches	Thick

DRILLING SYMBOLS



very loose	0-4
loose	5-10
medium dense	11-24
dense	25-50
very dense	>50

Consistency - Cohesive Soils	BPF
very soft	0-1
soft	2-4
firm	5-8
stiff	9-15
very stiff	16-30
hard	31-60
very hard	> 60

COLOR

blk	Black	wht	White
grn	Green	brn	Brown
orng	Orange	yel	Yellow
dk	Dark	lt	Light
IOS	Iron Oxide	Stained	-

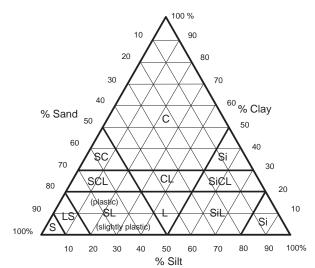
GRAIN SIZE /PLASTICITY

VF Very Fine	plPlastic
F Fine	slplSlightly
Cr Coarse	Plastic

SOIL/ROCK TERMS

C	. Clay	Lmst	Limestone
L	. Loam	Sst	Sandstone
S	. Sand	Dolo	Dolostone
Si	. Silt	wx	weathered
G	. Gravel (No. 7	10 Sieve t	o 3 inches)
Bldr Boulder (over 3 inches)			
T till (unsorted, nonstratified glacial			
deposits)			

Mn/DOT Triangular Textural Soil Classification System



WINNESD

OF TRP

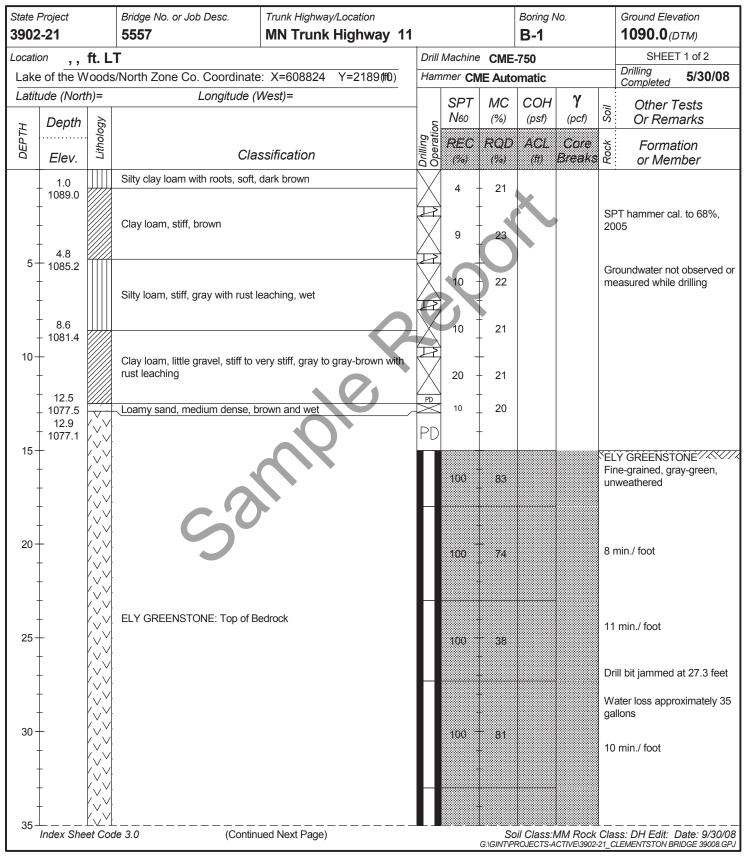
DEPAR

THEN

LABORATORY LOG & TEST RESULTS - SUBSURFACE EXPLORATION

UNIQUE NUMBER 70658

This boring was taken by STS Limited, Inc. under a consultant contract for Mn/DOT



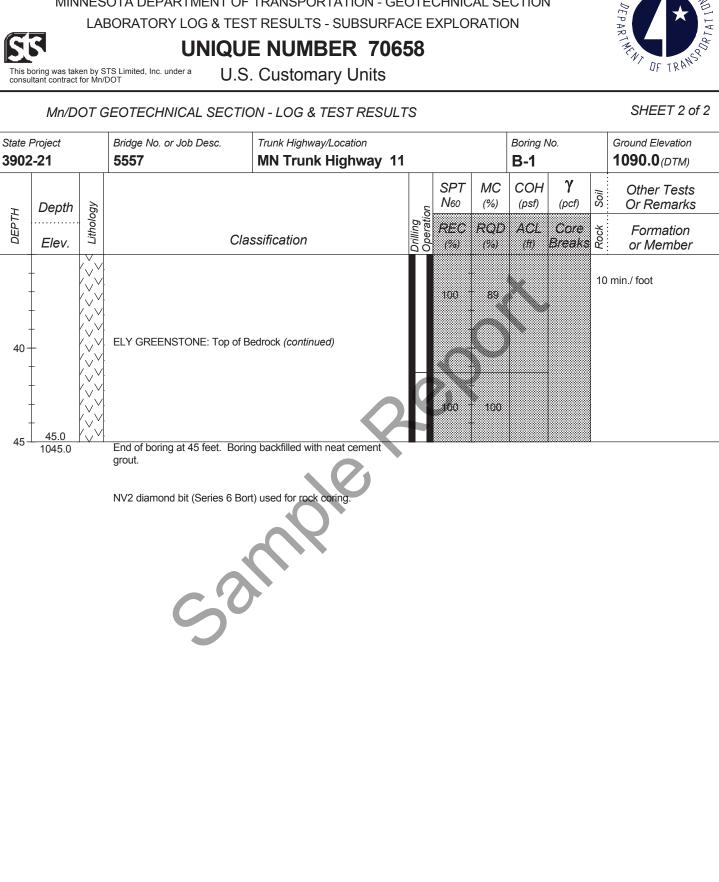
LABORATORY LOG & TEST RESULTS - SUBSURFACE EXPLORATION

This boring was taken by STS Limited, Inc. under a consultant contract for $\ensuremath{\mathsf{Mn/DOT}}$

DEPTH

40

45



WINNESD

LABORATORY LOG & TEST RESULTS - SUBSURFACE EXPLORATION

UNIQUE NUMBER 70659

This boring was taken by STS Limited, Inc. under a consultant contract for Mn/DOT

DEPTH

5

10

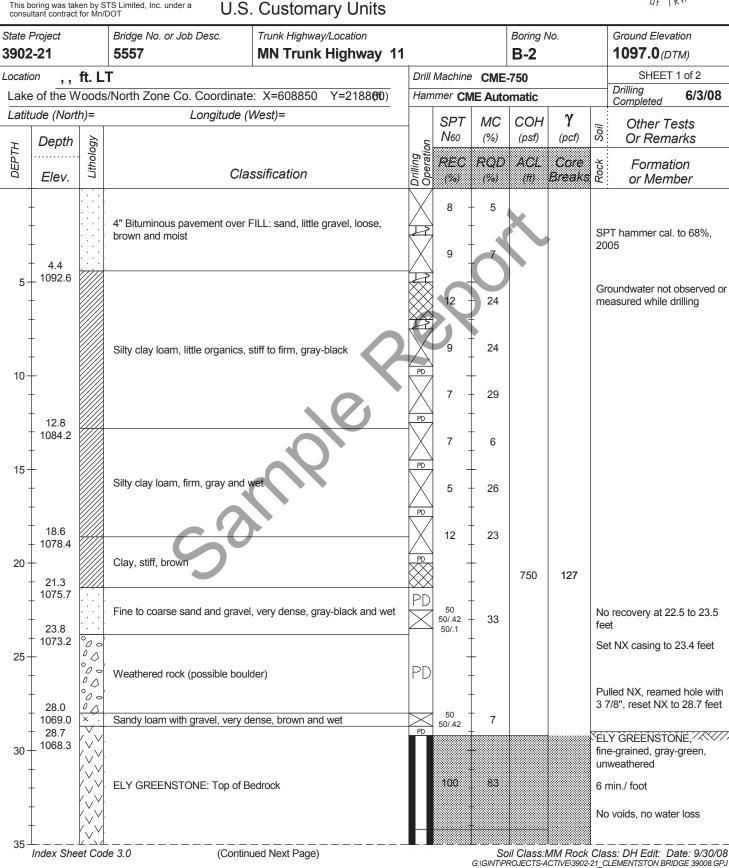
15

20

25

30

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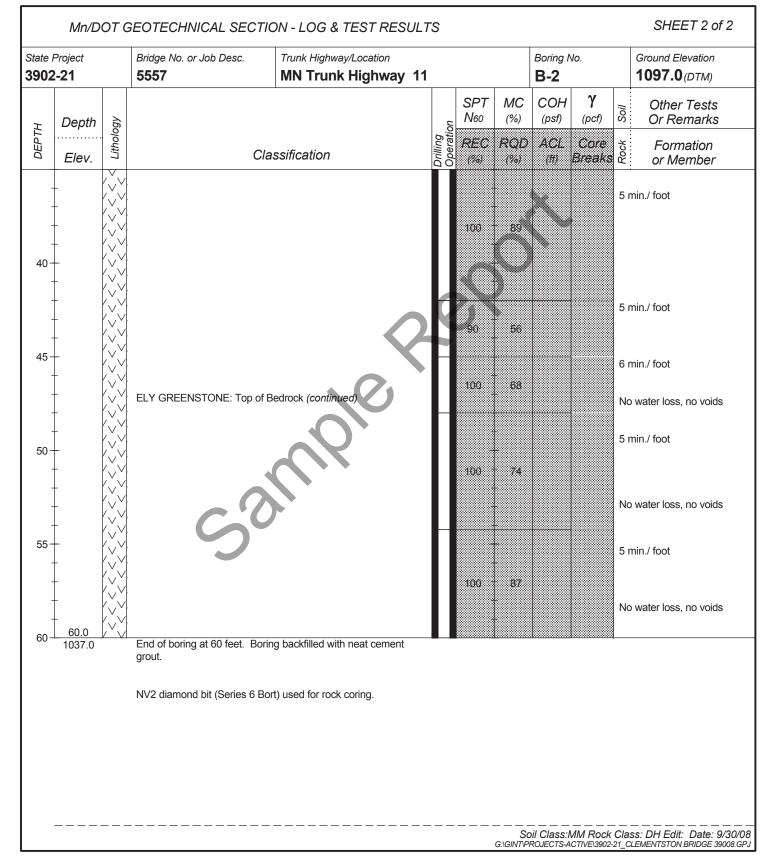




LABORATORY LOG & TEST RESULTS - SUBSURFACE EXPLORATION

UNIQUE NUMBER 70659

This boring was taken by STS Limited, Inc. under a consultant contract for $\ensuremath{\mathsf{Mn/DOT}}$



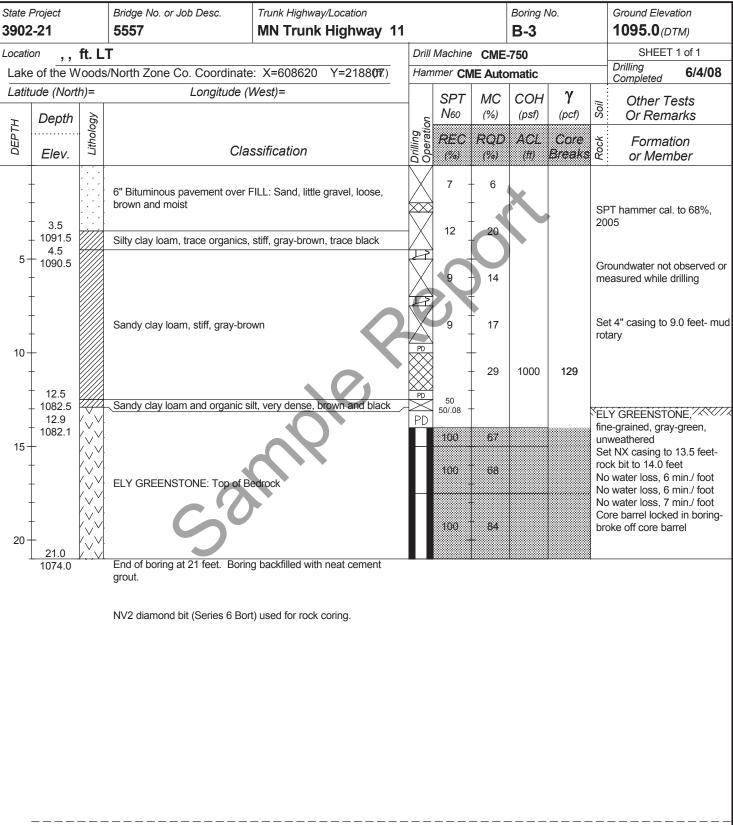


LABORATORY LOG & TEST RESULTS - SUBSURFACE EXPLORATION

UNIQUE NUMBER 70660

This boring was taken by STS Limited, Inc. under a consultant contract for Mn/DOT

U.S. Customary Units



Index Sheet Code 3.0

Soil Class: MM Rock Class: DH Edit: Date: 9/30/08 G:\GINT\PROJECTS-ACTIVE\3902-21_CLEMENTSTON BRIDGE 39008.GPJ



MINNESO

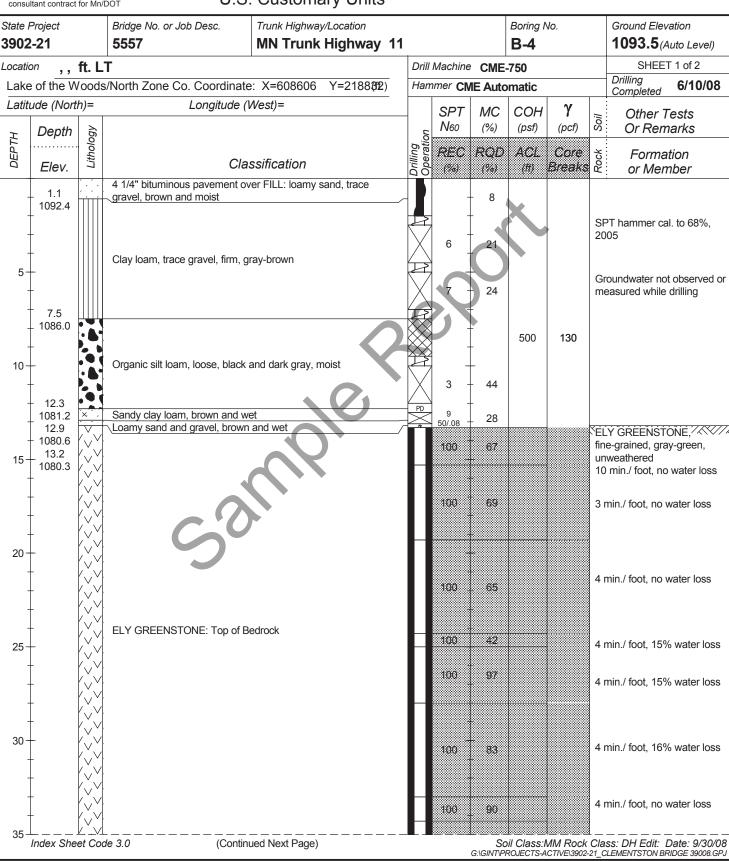
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LABORATORY LOG & TEST RESULTS - SUBSURFACE EXPLORATION

UNIQUE NUMBER 70661

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LABORATORY LOG & TEST RESULTS - SUBSURFACE EXPLORATION

UNIQUE NUMBER 70661

This boring was taken by STS Limited, Inc. under a consultant contract for $\ensuremath{\mathsf{Mn/DOT}}$

